

IN THE SPECIFICATION:

Page 2, lines 13-14, amend the table as follows:

| Component                      | % by weight    |
|--------------------------------|----------------|
| SiO <sub>2</sub>               | 55 - 62        |
| Al <sub>2</sub> O <sub>3</sub> | 13 - 17        |
| B <sub>2</sub> O <sub>3</sub>  | 0 - 2          |
| P <sub>2</sub> O <sub>5</sub>  | 1.5 - 3        |
| Li <sub>2</sub> O              | 0 - 2          |
| Na <sub>2</sub> O              | 7 - 12         |
| K <sub>2</sub> O               | 8 - 12         |
| MgO                            | 0 - 2          |
| CaO                            | 1 - <u>≤</u> 4 |
| BaO                            | 0 - 2          |
| Tb <sub>2</sub> O <sub>3</sub> | 0 - 3          |
| Me (IV) O <sub>2</sub>         | 0.5 - 3        |

Page 6:

Please replace Table 1 as filed with Table 1 as attached hereto.

Page 8, lines 1-10:

A comparison of the tests shows that the thermal expansion coefficient of the glass ceramic according to the invention is controllable. Thus, a thermal expansion coefficient (TEC) in the range of  $9.0$  to  $13.5 \times 10^{-6}$ , preferably  $10.5$  to  $12 \times 10^{-6}$ , can be set. In comparison to the ceramics known from EP 0 622 342 B1, which have either too low a TEC ( $\leq 11 \times 10^{-6}/K$ ) or a too high TEC ( $\geq 16 \times 10^{-6}/K$ ), the

TABLE I (Columns 1 - 12)

| Test  | Ivo.15  | 1       | 2     | 3     | 4       | 5     | 6     | 7      | 8       | 9      | 10      | 11      | 12     |
|---|---------|---------|-------|-------|---------|-------|-------|--------|---------|--------|---------|---------|--------|
| % by weight   |         |         |       |       |         |       |       |        |         |        |         |         |        |
| SiO <sub>2</sub>  | 55.34   | 59.78   | 59.05 | 60.01 | 58.03   | 56.22 | 59.83 | 55.53  | 58.44   | 58.93  | 58.02   | 59.08   | 58.72  |
| Al <sub>2</sub> O <sub>3</sub>  | 16.09   | 14.52   | 14.63 | 16.45 | 15.91   | 16.83 | 16.4  | 14.71  | 14.23   | 14.44  | 14.34   | 14.48   | 14.78  |
| B <sub>2</sub> O <sub>3</sub>   | 0.22    | 0.44    | 0.44  |       |         | 1.09  | 1.07  | 2.23   | 0.44    |        |         | 1.1     |        |
| P <sub>2</sub> O <sub>5</sub>   | 2.59    | 2.32    | 2.42  | 2.33  | 2.38    | 2.06  | 1.4   | 2.46   | 2.44    | 2.43   | 2.43    | 2.43    | 2.44   |
| Li <sub>2</sub> O   |         |         |       | 1.28  | 1.31    | 1.1   | 1.29  | 0.45   |         |        |         |         |        |
| Na <sub>2</sub> O   | 9.08    | 9.36    | 9.3   | 4.44  | 6.39    | 5.91  | 6     | 9.97   | 9.84    | 10.03  | 10.01   | 10.04   | 9.13   |
| K <sub>2</sub> O  | 11.88   | 9.09    | 9.23  | 13.49 | 12.96   | 13.11 | 12.86 | 10     | 9.63    | 9.21   | 9.15    | 9.24    | 10.19  |
| MgO   |         |         |       |       |         |       |       |        |         |        |         |         |        |
| CaO   | 2.6     | 2.97    | 2.95  | 0.09  | 1.3     | 1.91  | 0.09  | 2.88   | 2.98    | 2.97   | 2.97    | 2.97    | 2.97   |
| BaO   |         |         |       |       |         |       |       |        |         |        |         |         |        |
| Tb <sub>2</sub> O <sub>3</sub>  |         |         |       |       |         |       |       |        |         |        |         |         |        |
| SnO <sub>2</sub>  | 1.52    | 0.88    | 0.85  | 0.86  | 0.87    |       |       | 1.45   | 0.89    | 0.88   | 0.88    | 1.43    | 1.44   |
| CeO <sub>2</sub>  |         | 1.1     | 1.06  | 0.86  | 0.87    | 1.07  | 0.33  | 1.11   | 1.1     | 1.1    | 1.1     | 0.33    | 0.33   |
| ZrO <sub>2</sub>  | 1.9     |         |       |       |         |       |       |        |         |        |         |         |        |
| TiO <sub>2</sub>  | 0.3     |         |       |       |         |       |       |        |         |        |         |         |        |
| Calculated thermal expansion coefficient (Alpha x10 <sup>exp. -6/K)</sup> |         |         |       |       |         |       |       |        |         |        |         |         |        |
|   | 10.73   | 9.91    | 9.98  | 9.64  | 10.53   | 10.23 |       | 9.96   | 10.58   | 10.35  | 10.31   | 10.02   | 10.32  |
| Applicable relevant baking temperature in °C                              |         |         |       |       |         |       |       |        |         |        |         |         |        |
|   | 960     | 940     | 940   | 980   | 920     | 940   | 940   | 870    | 920     | 940    | 920     | 940     | 950    |
| Tempering of the glass frit (Min./°C)                                     |         |         |       |       |         |       |       |        |         |        |         |         |        |
|   | 60/950  | 30/950  | 30/95 | 950   | 30/950  |       |       | 30/950 | 30/980  | 30/930 | 30/960  | 30/940  | 60/950 |
| Measured thermal expansion coefficient                                    |         |         |       |       |         |       |       |        |         |        |         |         |        |
|   | unknown | unknown | 9.71  |       | unknown |       |       | 17     | unknown | 12.01  | unknown | unknown | 11.08  |
| Optical values  |         |         |       |       |         |       |       |        |         |        |         |         |        |
| L*tran  | 69.7    | 77.1    | 76.6  |       | cloudy  |       |       | 81.4   | 65.8    | 79.8   | 80.5    | 80.9    | 81     |
| b*tran  | 26.5    | 31.6    | 32.8  |       |         |       |       | 9.4    | 27.4    | 25.6   | 29.3    | 34.9    | 30.3   |
| s.  |         |         |       |       |         |       |       |        |         |        |         |         | 32.9   |
| b*ref.  |         |         |       |       |         |       |       |        |         |        |         |         |        |

glass ceramic according to the invention can be set in the TEC range of  $11.0$  to  $13.0 \times 10^{-6}/K$  for coating ceramics, which is especially important in the dental field.

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